Bus Admittance Matrix or Y_{bus}

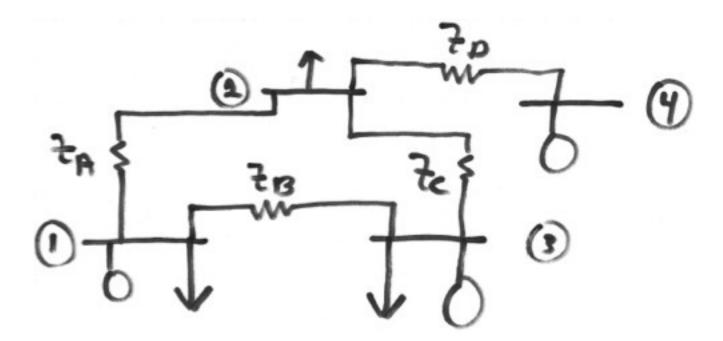
- FIRST STEP IN SOLVING THE POWER FLOW IS TO CREATE WHAT IS KNOWN AS THE BUS ADMITTANCE MATRIX, OFTEN CALL THE Y_{BUS}.
- THE Y_{BUS} GIVES THE RELATIONSHIPS BETWEEN ALL THE BUS CURRENT INJECTIONS, I, AND ALL THE BUS VOLTAGES, V,

$$I = Y_{RUS} V$$

 THE Y_{BUS} IS DEVELOPED BY APPLYING KCL AT EACH BUS IN THE SYSTEM TO RELATE THE BUS CURRENT INJECTIONS, THE BUS VOLTAGES, AND THE BRANCH IMPEDANCES AND ADMITTANCES

Y_{bus} Example

Determine the bus admittance matrix for the network shown below, assuming the current injection at each bus i is $I_i = I_{Gi} - I_{Di}$ where I_{Gi} is the current injection into the bus from the generator and I_{Di} is the current flowing into the load



By KCL at bus 1 we have

$$I_{1} @ I_{G1} - I_{D1}$$

$$I_{1} = I_{12} + I_{13} = \frac{V_{1} - V_{2}}{Z_{A}} + \frac{V_{1} - V_{3}}{Z_{B}}$$

$$I_{1} = (V_{1} - V_{2})Y_{A} + (V_{1} - V_{3})Y_{B} \qquad (\text{with } Y_{j} = \frac{1}{Z_{j}})$$

$$= (Y_{A} + Y_{B})V_{1} - Y_{A}V_{2} - Y_{B}V_{3}$$

Similarly

$$\begin{split} I_2 &= I_{21} + I_{23} + I_{24} \\ &= -Y_A V_1 + (Y_A + Y_C + Y_D) V_2 - Y_C V_3 - Y_D V_4 \end{split}$$

We can get similar relationships for buses 3 and 4. The results can then be expressed in matrix form

$$\begin{bmatrix} I_1 \\ I_2 \\ I_3 \\ I_4 \end{bmatrix} = \begin{bmatrix} Y_A + Y_B & -Y_A & -Y_B & 0 \\ -Y_A & Y_A + Y_C + Y_D & -Y_C & -Y_D \\ -Y_B & -Y_C & Y_B + Y_C & 0 \\ 0 & -Y_D & 0 & Y_D \end{bmatrix} \begin{bmatrix} V_1 \\ V_2 \\ V_3 \\ V_4 \end{bmatrix}$$

For a system with n buses, Y_{bus} is an n by n symmetric matrix (i.e., one where $A_{ij} = A_{ji}$)

Y_{BUS} GENERAL FORM

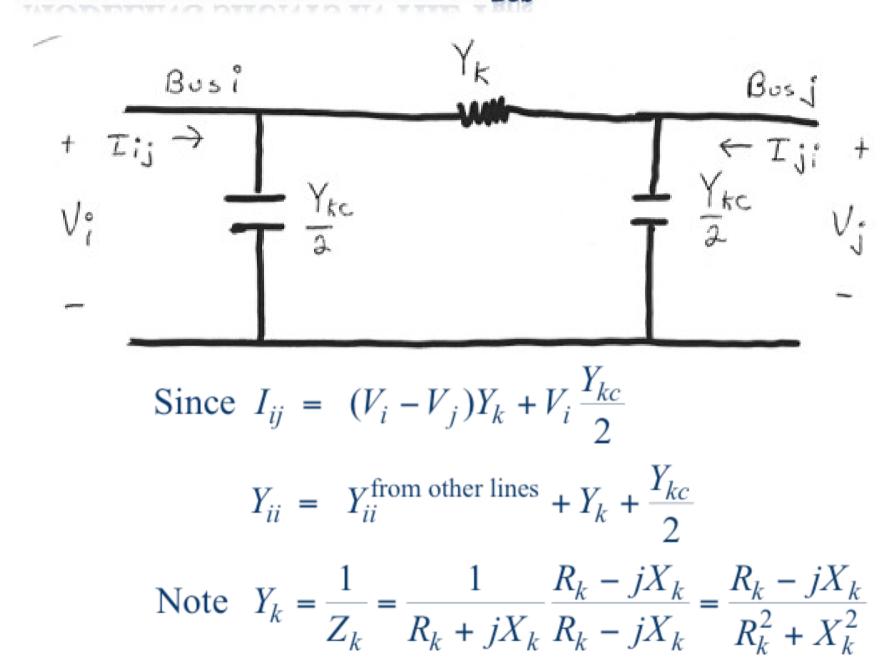
The diagonal terms, Y_{ii} , are the self admittance terms, equal to the sum of the admittances of all devices incident to bus i.

The off-diagonal terms, Y_{ij} , are equal to the negative of the sum of the admittances joining the two buses.

With large systems Y_{bus} is a sparse matrix (that is, most entries are zero)

Shunt terms, such as with the π line model, only affect the diagonal terms.

MODELING SHUNTS IN THE YBUS



Two Bus System Example

$$I_{1} = \frac{(V_{1} - V_{2})}{Z} + V_{1} \frac{Y_{c}}{2} \qquad \frac{1}{0.03 + j0.04} = 12 - j16$$

$$\begin{bmatrix} I_{1} \\ I_{2} \end{bmatrix} = \begin{bmatrix} 12 - j15.9 & -12 + j16 \\ -12 + j16 & 12 - j15.9 \end{bmatrix} \begin{bmatrix} V_{1} \\ V_{2} \end{bmatrix}$$

Using the Y_{bus}

If the voltages are known then we can solve for the current injections:

$$\mathbf{Y}_{bus}\mathbf{V}=\mathbf{I}$$

If the current injections are known then we can solve for the voltages:

$$\mathbf{Y}_{bus}^{-1}\mathbf{I} = \mathbf{V} = \mathbf{Z}_{bus}\mathbf{I}$$

where \mathbf{Z}_{bus} is the bus impedance matrix

Solving for Bus Currents

For example, in previous case assume

$$\mathbf{V} = \begin{bmatrix} 1.0 \\ 0.8 - j0.2 \end{bmatrix}$$

Then

$$\begin{bmatrix} 12 - j15.9 & -12 + j16 \\ -12 + j16 & 12 - j15.9 \end{bmatrix} \begin{bmatrix} 1.0 \\ 0.8 - j0.2 \end{bmatrix} = \begin{bmatrix} 5.60 - j0.70 \\ -5.58 + j0.88 \end{bmatrix}$$

Therefore the power injected at bus 1 is

$$S_1 = V_1 I_1^* = 1.0 \times (5.60 + j0.70) = 5.60 + j0.70$$

 $S_2 = V_2 I_2^* = (0.8 - j0.2) \times (-5.58 - j0.88) = -4.64 + j0.41$

Solving for Bus Voltages

For example, in previous case assume

$$\mathbf{I} = \begin{bmatrix} 5.0 \\ -4.8 \end{bmatrix}$$

Then

$$\begin{bmatrix} 12 - j15.9 & -12 + j16 \\ -12 + j16 & 12 - j15.9 \end{bmatrix}^{-1} \begin{bmatrix} 5.0 \\ -4.8 \end{bmatrix} = \begin{bmatrix} 0.0738 - j0.902 \\ -0.0738 - j1.098 \end{bmatrix}$$

Therefore the power injected is

$$S_1 = V_1 I_1^* = (0.0738 - j0.902) \times 5 = 0.37 - j4.51$$

 $S_2 = V_2 I_2^* = (-0.0738 - j1.098) \times (-4.8) = 0.35 + j5.27$

Power Flow Analysis

- When analyzing power systems we know neither the complex bus voltages nor the complex current injections
- Rather, we know the complex power being consumed by the load, and the power being injected by the generators plus their voltage magnitudes
- Therefore we can not directly use the Y_{bus} equations, but rather must use the power balance equations

Power Balance Equations

From KCL we know at each bus i in an n bus system the current injection, I_i , must be equal to the current that flows into the network

$$I_i = I_{Gi} - I_{Di} = \sum_{k=1}^n I_{ik}$$

Since $I = Y_{bus}V$ we also know

$$I_i = I_{Gi} - I_{Di} = \sum_{k=1}^n Y_{ik} V_k$$

The network power injection is then $S_i = V_i I_i^*$

Power Balance Equations

$$S_i = V_i I_i^* = V_i \left(\sum_{k=1}^n Y_{ik} V_k \right)^* = V_i \sum_{k=1}^n Y_{ik}^* V_k^*$$

This is an equation with complex numbers.

Sometimes we would like an equivalent set of real power equations. These can be derived by defining

$$Y_{ik} @ G_{ik} + jB_{ik}$$

$$V_i @ |V_i|e^{j\theta_i} = |V_i| \angle \theta_i$$

$$\theta_{ik} @ \theta_i - \theta_k$$

Recall $e^{j\theta} = \cos\theta + j\sin\theta$

Real Power Balance Equations

$$S_{i} = P_{i} + jQ_{i} = V_{i} \sum_{k=1}^{n} Y_{ik}^{*} V_{k}^{*} = \sum_{k=1}^{n} |V_{i}| |V_{k}| e^{j\theta_{ik}} (G_{ik} - jB_{ik})$$

$$= \sum_{k=1}^{n} |V_{i}| |V_{k}| (\cos \theta_{ik} + j \sin \theta_{ik}) (G_{ik} - jB_{ik})$$

Resolving into the real and imaginary parts

$$P_{i} = \sum_{k=1}^{n} |V_{i}| |V_{k}| (G_{ik} \cos \theta_{ik} + B_{ik} \sin \theta_{ik}) = P_{Gi} - P_{Di}$$

$$Q_{i} = \sum_{k=1}^{n} |V_{i}| |V_{k}| (G_{ik} \sin \theta_{ik} - B_{ik} \cos \theta_{ik}) = Q_{Gi} - Q_{Di}$$

Power Flow Requires Iterative Solution

In the power flow we assume we know S_i and the Y_{bus} . We would like to solve for the V's. The problem is the below equation has no closed form solution:

$$S_i = V_i I_i^* = V_i \left(\sum_{k=1}^n Y_{ik} V_k \right)^* = V_i \sum_{k=1}^n Y_{ik}^* V_k^*$$

Rather, we must pursue an iterative approach.