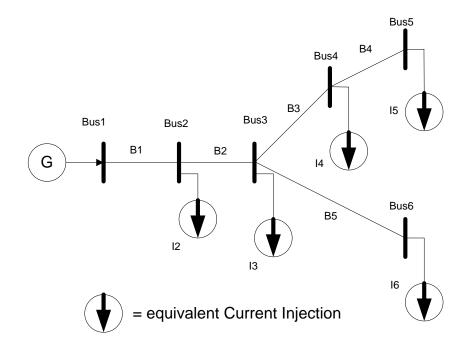
# A NETWORK TOPOLOGY BASED THREE PHASE LOAD FLOW

(Balanced system)



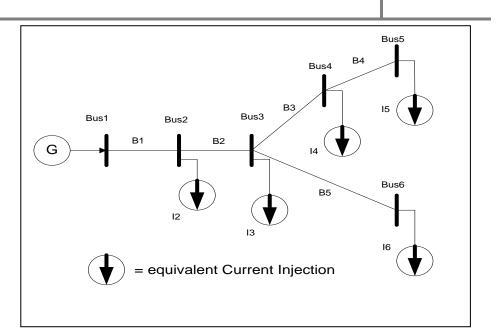
Step 1:

Build the Bus-Injection to Branch-Current (**BIBC**) matrix.

B1, B2, .... B6. Is branch current.

Look at the figure.

 $B_{5} = I_{6}$   $B_{4} = I_{5}$   $B_{3} = I_{4} + I_{5}$   $B_{2} = I_{4} + I_{5} + I_{6}$   $B_{1} = I_{2} + I_{3} + I_{4} + I_{5} + I_{6}$ 



Furthermore, **BIBC** matrix can be obtained as

$\begin{bmatrix} B_1 \end{bmatrix}$		г1	1	1	1	ן1	$\begin{bmatrix} I_2 \\ I_3 \end{bmatrix}$
<i>B</i> <sub>2</sub>		0	1	1	1	1	$I_3$
$B_3$	=	0	0	1	1	0	$I_4 \\ I_5 \\ I_6$
$B_4$		0	0	0	1	0	$I_5$
$B_5$		L0	0	0	0	1 <b>J</b>	$\lfloor I_6 \rfloor$

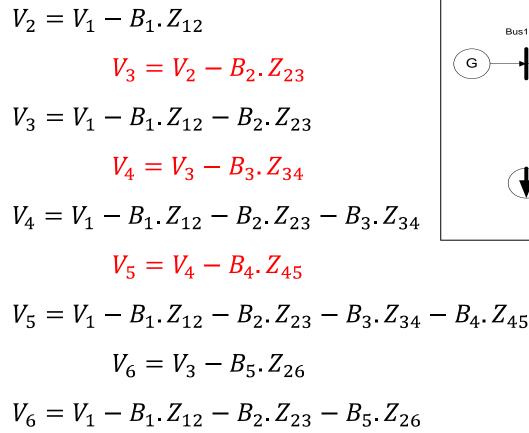
Can be expressed in the general form as

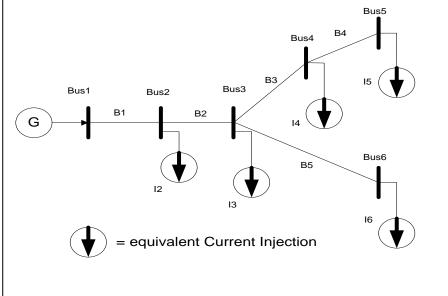
 $[B] = [BIBC][I] \dots (1)$ 

Step2.

Build Branch-Current to Bus-Voltage (BCBV) matrix.

Look at the figure:





$$V_{1} - V_{2} = B_{1} \cdot Z_{12}$$

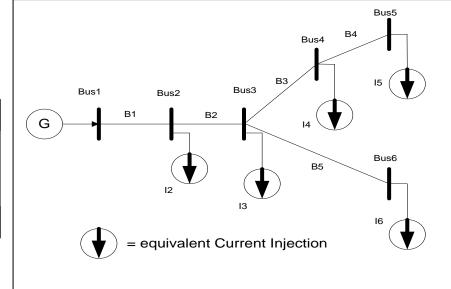
$$V_{1} - V_{3} = B_{1} \cdot Z_{12} + B_{2} \cdot Z_{23}$$

$$V_{1} - V_{4} = B_{1} \cdot Z_{12} + B_{2} \cdot Z_{23} + B_{3} \cdot Z_{34}$$

$$V_{1} - V_{5} = B_{1} \cdot Z_{12} + B_{2} \cdot Z_{23} + B_{3} \cdot Z_{34} + B_{4} \cdot Z_{45}$$

$$V_{1} - V_{6} = B_{1} \cdot Z_{12} + B_{2} \cdot Z_{23} + B_{5} \cdot Z_{36}$$

$$\begin{bmatrix} V_{1} - V_{2} \\ V_{1} - V_{3} \\ V_{1} - V_{4} \\ V_{1} - V_{5} \\ V_{1} - V_{6} \end{bmatrix} = \begin{bmatrix} Z_{12} & 0 & 0 & 0 & 0 \\ Z_{12} & Z_{23} & 0 & 0 & 0 \\ Z_{12} & Z_{23} & Z_{34} & 0 & 0 \\ Z_{12} & Z_{23} & Z_{34} & Z_{45} & 0 \\ Z_{12} & Z_{23} & 0 & 0 & Z_{36} \end{bmatrix} \begin{bmatrix} B_{1} \\ B_{2} \\ B_{3} \\ B_{4} \\ B_{5} \end{bmatrix}$$
Rewriting in the general form, we have



 $[\Delta V] = [BCBV][B] \dots \dots \dots \dots \dots (2)$ 

Substituted (1) to (2), we get  $[\Delta V] = [BCBV][BIBC][I].....(3)$  $[\Delta V] = [DLF][I] ....(4)$ 

Step3.

Follow the algorithm.

- 1. Input data.
- 2. Build **BIBC** matrix.
- 3. Build BCBV matrix.
- 4. Build **DLF** matrix.
- 5. Iteration k=0.
- 6. Iteration k=k+1.

7. Solve for three-phase power flow by using

$$I_i^k = \left(\frac{P_i + jQ_i}{V_i^k}\right)^s$$

And

 $[\Delta V^{k}] = [DLF][I^{k}]$ And update voltages.  $[V^{k+1}] = [Vno\_load] - [\Delta V^{k}]$ 

- 8. If  $max_i(|I_i^{k+1}| |I_i^k|) > tolerance$ , go to (6)
- 9. Report and end.

Reference:

 Jen-Hao TENG, "A Network-Topology-based Three-Phase Load Flow for Distribution Systems", Proc. Natl.Sci.Counc. ROC(A) Vol.24, No. 4,2000.pp.259-264

## **ANOTHER METHOD TO BUILD BIBC MATRIX**

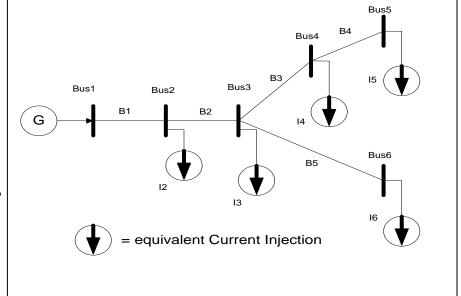
1. Branch-path incidence matrix

The branch-path incidence matrix also called **K-Matrix** 

```
BIBC Matrix = - [K-Matrix]
```

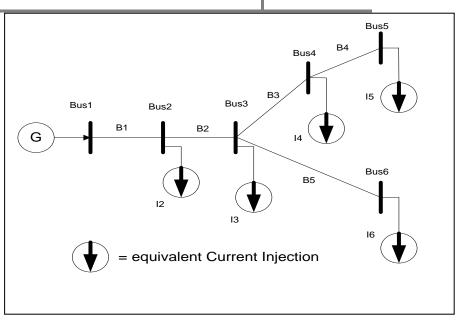
### The elements of K-Matrix are:

- Row element is number of branch
- Column element is number of buses (exclude of reference bus)



The principles of building branch-path incidence matrix (K-Matrix) is Find the path from the bus go to the reference K (i, j) = +1 if the branch *i* is in the path from the bus *j* to the reference node and directed in the same direction.

K (i, j) = -1 if the branch *i* is in the path from the bus *j* to the reference node and directed in the opposite direction.



	bus2	bus3	bus4	bus5 b	us6
<i>B</i> 1				-1	
<i>B</i> 2	0	-1	-1	-1	-1
K = B3	0	0	-1	-1	0
<i>B</i> 4	0	0	0	-1	0
<i>B</i> 5	LO	0	0	0	_1

$$BIBC = -K = -\begin{bmatrix} -1 & -1 & -1 & -1 & -1 \\ 0 & -1 & -1 & -1 & -1 \\ 0 & 0 & -1 & -1 & 0 \\ 0 & 0 & 0 & -1 & 0 \\ 0 & 0 & 0 & 0 & -1 \end{bmatrix} = \begin{bmatrix} 1 & 1 & 1 & 1 & 1 \\ 0 & 1 & 1 & 1 & 1 \\ 0 & 1 & 1 & 1 & 1 \\ 0 & 0 & 1 & 1 & 0 \\ 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & 1 \end{bmatrix}$$

#### **RELATIONSHIP BETWEEN** *BIBC* **MATRIX AND** *BCBV* **MATRIX**

• Look at K-Matrix

	bus2	bus3	bus4	bus5 bu	us6
B1	г—1	-1	-1	-1	ר1–
<i>B</i> 2		-1	-1	-1	-1
K = B3	0	0	-1	-1	0
<i>B</i> 4	0	0	0	-1	0
<i>B</i> 5	LO	0	0	0	_1

If we transpose the K-Matrix, we have

$$K' = bus2 \begin{bmatrix} -1 & 0 & 0 & 0 & 0 \\ bus3 & \begin{bmatrix} -1 & -1 & 0 & 0 & 0 & 0 \\ -1 & -1 & -1 & 0 & 0 & 0 \\ -1 & -1 & -1 & -1 & 0 & 0 \\ -1 & -1 & -1 & -1 & -1 & 0 \\ bus6 & \begin{bmatrix} 1 & 0 & 0 & 0 & 0 \\ -1 & -1 & 0 & 0 & -1 \end{bmatrix}$$
$$B1 = B2 = B3 = B4 = B5$$
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$$B5 = B4 = B5$$
$$B1 = B4 = B4 = B4$$
$$B5 = B4 = B5$$
$$B1 = B4 = B4 = B4$$
$$B5 = B4 = B4$$

Because

BIBC = -KSo BIBC' = -K'

# Compare *BIBC*' with BCBV

	<i>B</i> 1	<i>B</i> 2	<i>B</i> 3	<i>B</i> 4	<i>B</i> 5
bus2	۲٦	0	0	0	ך0
bus3	1	1	0	0	0
BIBC' = bus4	1	1	1	0	0
bus5	1	1	1	1	0
bus6	L <sub>1</sub>	1	0	0	1]

$$BCBV = \begin{bmatrix} Z_{12} & 0 & 0 & 0 & 0 \\ Z_{12} & Z_{23} & 0 & 0 & 0 \\ Z_{12} & Z_{23} & Z_{34} & 0 & 0 \\ Z_{12} & Z_{23} & Z_{34} & Z_{45} & 0 \\ Z_{12} & Z_{23} & 0 & 0 & Z_{36} \end{bmatrix}$$

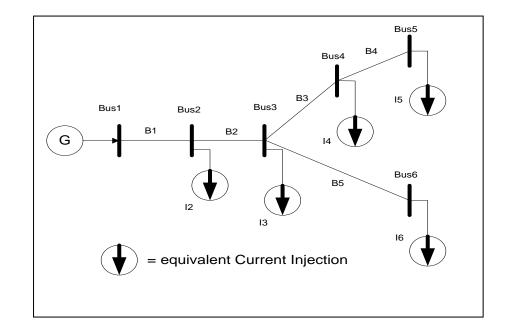
$$Z_{12} = impedance in branch B1$$

$$Z_{23} = impedance in branch B2$$

$$Z_{34} = impedance in branch B3$$

$$Z_{45} = impedance in branch B4$$

$$Z_{36} = impedance in branch B5$$



Reference:

- 1. Jen-Hao TENG, "A Network-Topology-based Three-Phase Load Flow for Distribution Systems", Proc. Natl.Sci.Counc. ROC(A) Vol.24, No.4,2000.pp.259-264
- T.-H. Chen, N.-C.Yang, "Three-phase power-flow by direct Zbr method for unbalanced radial distribution systems", IET Gener.Transm.Distrib., 2009,Vol.3, Iss.10,pp.903-910.